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Design of an Assisted Photovoltaic Solar Energy System for Block 5

Diseño de un Sistema de Energía Solar Fotovoltaica Asistido para el Bloque 5

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Abstract

This study focuses on the design of a photovoltaic system to supply electricity to the building "Block 5" of the FACI - UTLVTE. This design considers obtaining energy through two sources which are photovoltaic modules and the local power grid. Therefore, the designed photovoltaic system is conceived as an assisted solar photovoltaic installation. In the present research, calculations and simulations are carried out based on an analysis of the load demand and meteorological data obtained with PVsyst software. The results obtained indicate that the designed photovoltaic system can support a percentage of the demand of the lighting circuits, general outlets and special loads of Block 5, which corresponds to a decrease in the costs associated with the consumption of electricity from the local power grid. These results demonstrate that the sizing achieved by this photovoltaic system is optimal, which is validated by means of the PVsyst software.

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Keywords: solar resource analysis, PVsyst, photovoltaic system, demand estimation.

Resumen

Este estudio se centra en el diseño de un sistema fotovoltaico que sirva para abastecer con electricidad al edificio "Bloque 5" de la FACI - UTLVTE. Este diseño considera la obtención de energía a través de dos fuentes que son unos módulos fotovoltaicos y la red eléctrica local. Por lo tanto, el sistema fotovoltaico diseñado se concibe como una instalación solar fotovoltaica de tipo asistida. En la presente investigación, se llevan a cabo cálculos y simulaciones basados en un análisis de la demanda de las cargas y datos meteorológicos obtenidos con el software PVsyst. Los resultados obtenidos indican que el sistema fotovoltaico diseñado puede soportar un porcentaje de la demanda de los circuitos de iluminación, tomacorrientes generales y cargas especiales del Blogue 5, lo que corresponde a una disminución de los costos asociados con el consumo de energía eléctrica proveniente de la red eléctrica local. Dichos resultados demuestran que el dimensionamiento alcanzado por este sistema fotovoltaico es óptimo, lo cual es validado mediante el software PVsyst.

Palabras clave: análisis del recurso solar, PVsyst, sistema fotovoltaico, estimación de la demanda.

Introduction

Photovoltaic systems harness solar energy, an inexhaustible source of energy, so the implementation of this type of energy system helps to move towards a more sustainable energy matrix. Likewise, designing these systems fosters innovation and technological progress, since it contributes to the understanding of how to efficiently deliver nonconventional energy to places that require it, a concept known as "distributed generation". At present, the power supply of FACI's "Block 5" building (Figure 1) depends exclusively on CNEL EP's distribution network. The cost generated by the consumption of energy from a public network in a building with the characteristics of Block 5 can be high. One solution to this problem, which would help reduce the costs associated with energy consumption, is the development of an assisted photovoltaic system that injects solar renewable energy into the building and can also receive energy from the available electrical grid when necessary. The implementation of such a system can be beneficial not only from an economic but also from an environmental point of view.

The objective of this article is to reveal the design of a photovoltaic power generation system for Block 5 of the FACI, where the key components of this system (i.e. inverter and photovoltaic modules) are technically defined or specified, and the feasibility of the solar installation is evaluated from the point of view of the solar resource available at the location of Block 5, while taking into account the demand of the load installed in the building. At the end, a bill of materials and a budget for the implementation of this photovoltaic system is estimated.

Figure 1. Building Block 5 - FACI - UTLVTE.



Note. Taken from (Cagua, 2023).

Methodology

Figure 2 presents the two basic types of PV systems, which are: a) Offgrid installations, and b) Grid-connected installations. The choice of one or the other type of PV configuration depends on the application; for example, grid-connected solar installations are used when the objective is to sell electricity and/or perform self-consumption, while off-grid installations are generally used in rural electrification, pumping, signaling, and communications applications (Baselga-Carreras, 2019).. In the technical instruction ITC-BT-40 of the Spanish Low Voltage Electrotechnical Regulation, a third classification or type of photovoltaic system called Photovoltaic Assisted Solar Installation arises, which has an additional source of energy, i.e., it has photovoltaic modules that are used to feed the load (Figure 3) (Mascarós-Mateo, 2016) and the energy from the photovoltaic modules is complemented with the energy from the local power grid. This article focuses on the design of an assisted photovoltaic installation for Block 5, whose implementation will reduce the consumption of electricity from the local grid, supplying energy to the building by means of a complementary source based on photovoltaic solar energy.

Figure 2. Basic photovoltaic systems: (a) Isolated, (b) Gridinterconnected.





Note. Taken from (Castejón & Herranz, 2010)..



Figure 3. Assisted photovoltaic system

Finally, it is necessary to mention that the main components in PV systems are usually the PV modules and the inverter. However, it is common that some of the following components are also required in a photovoltaic system, depending on the type of application (Cagua, 2023)Photovoltaic modules, inverter, rechargeable batteries (accumulator), charge controller or regulator, junction boxes (combiners), mounting structure, energy meter, automatic disconnection switches (electrical protections), wiring and monitoring system.

FACI's Block 5 building has three floors with classrooms, staff rooms and a small bar. From a survey of information, it has been established in Tables 1, 2 and 3 that the electrical load of this building, composed of lighting fixtures, general outlets and special loads (e.g. air conditioning, electric oven, etc.), demands a total estimated power of 3015 W + 14800 W + 25000 W = 42815 W. However, this total power value represents a maximum load demand value that, under normal building operating conditions, will most likely not occur. Then, in order to estimate a demand that probabilistically would be more in line with reality, the demand factors (DF) presented in Tables 4 and 5,

Note. Taken from (Mascarós-Mateo, 2016)..

established according to the Ecuadorian Construction Standard (NEC), are used. (Fernández & Fernández, 2022; Unamo et al., 2018)..

		Electrical Power -	Luminaires		
		El	ectrical Circ	cuit	
Zones	Environments	Device	Quantity	Watts per Device [W]	Power [W]
	Classroom 1	Fluorescent tube	12	18	216
oor	Classroom 2	Fluorescent tube	12	18	216
nd fl	Classroom 3	Fluorescent tube	12	18	216
Secc	Aisle	Fluorescent tube	16	18	288
	Food Bar	Led Spotlight	1	9	9
5	Classroom 1	Fluorescent tube	12	18	216
floc	Classroom 2	Fluorescent tube	12	18	216
pu	Classroom 3	Fluorescent tube	12	18	216
eco	Classroom 4	Fluorescent tube	12	18	216
S	Aisle	Fluorescent tube	14	18	252
	Teachers' lounge #2	Fluorescent tube	12	18	216
oor	Teachers' lounge #3	Fluorescent tube	10	18	180
Ч Ц	Teachers' lounge #4	Fluorescent tube	12	18	216
Thir	Bathrooms	Led Spotlight	2	9	18
	Aisle	Fluorescent tube	18	18	324
				Total Power (W)	3015

Table 1. Electrical power: Luminaires

 Table 2. Electrical power: General outlets

		Electrical Powe	er - Outlets				
		Ele	Electrical Circuit				
Zones	Environments	Dovico	Quantity	Watts per Device			
		Device	Quantity	[W]			
oor	Classroom 1	110 V outlet	3	200	600		
d fi	Classroom 2	110 V outlet	3	200	600		
ŭ	Classroom 3	110 V outlet	3	200	600		
Sec	Food Bar	110 V outlet	2	200	400		

DO	Classroom 1	110 V outlet	3	200	600	
d flo	Classroom 2	110 V outlet	3	200	600	
cone	Classroom 3	110 V outlet	3	200	600	
Sec	Classroom 4	110 V outlet	3	200	600	
oor	Teachers' lounge #2	110 V outlet	17	200	3400	
Third fl	Teachers' lounge #3	110 V outlet	17	200	3400	
	Teachers' lounge #4	110 V outlet	17	200	3400	
				Total Power (W)	14800	

Note. Taken from (Cagua, 2023).

Table 3. Electrical	power: Specia	l loads
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	Electrical Power - Special Loads							
		Electrical Circuit						
Zones	Environments	Device	Quantity	Watts per Device [W]	Power [W]			
σ.	Classroom 1	220 V power socket - Air conditioning	1	2500	2500			
econ floor	Classroom 2	220 V power socket - Air conditioning	1	2500	2500			
°,	Classroom 3	220 V power socket - Air conditioning	1	2500	2500			
ŗ	Classroom 1	220 V power socket - Air conditioning	1	2500	2500			
d flo	Classroom 2	220 V power socket - Air conditioning	1	2500	2500			
cone	Classroom 3	220 V power socket - Air conditioning	1	2500	2500			
Se	Classroom 4	220 V power socket - Air conditioning	1	2500	2500			
oc	Teachers' lounge #2	220 V power socket - Air conditioning	1	2500	2500			
Third flo	Teachers' lounge #3	220 V power socket - Air conditioning	1	2500	2500			
	Teachers' lounge #4	220 V power socket - Air conditioning	1	2500	2500			
				Total Power (W)	25000			

Note. Taken from (Cagua, 2023).

|--|

Housing Type	FD Lighting	FD Outlets
Small - Medium	0,70	0,50
Medium Large - Large	0,55	0,40
Special	0,53	0,30

Note. Based on. (Fernandez & Fernandez, 2022; Unamo et al., 2018)..

F	or one load	For two or more loads	For two or more loads	For two or more loads		
	1	CE<10 kW	10 kW <ce<20kw< td=""><td>CE>20kW</td></ce<20kw<>	CE>20kW		
	Ι	0.8	0.75	0.65		
Note. Based on. (Fernandez & Fernandez, 2022; Unamo et al., 20 Next, according to the type of load, Table 6 presents the pc demand values of Block 5 modified with the respective demand fa						
		(DF). (Cagua, 2	(DF). (Cagua, 2023):			
	Table 6.Total demand calculation for Block 5 usidemand factor.			ock 5 using the respective		
No	Type of cargo	Power [M/]		Demand with $FD =$		
	Type of cargo	FOWEI [VV]	FD	Power x FD [W].		
1	Luminaires	3015	0,53	1598		
2	Outlets	14800	0,53	7844		
3	Special loads	25000	0,65	16250		
			Total Demand with FD [W]	25692		

Table 5. Demand factors: Special loads.

Note. Taken from (Cagua, 2023).

Probabilistically, the value of 25692 W of total demand presented in Table 6 is more accurate than the previously mentioned 42815 W that established the value of the total power demand for building Block 5 assuming the unlikely case that the building load remains working at full load throughout the day. This power demand of 25692 W for Block 5, calculated using the respective demand factors, is the one that is subsequently used in the sizing of the PV field required for the solar installation of this building.

Solar Resource Study

In the literature. (Cevallos-Sierra & Ramos-Martin, 2018; Ulloa-Santillán, 2020) it is established that for a solar photovoltaic installation to be feasible from the point of view of the available solar resource and energy generation, it is necessary that the average annual value of the Global Horizontal Solar Irradiance (GHI - acronym in English) at the installation site is not less than 3.8 kWh/m2. With respect to the above, it has been identified through the PVsyst software, that for the location of Block 5, whose coordinates are latitude 0.9721 and longitude -79.6662, the GHI value is on average 4.94 kWh/m2/day (Figure 4), which indicates that, from the point of view of available solar resource and photovoltaic energy production, the implementation of a photovoltaic system is viable in this location.

Figure 4. Annual average of Global Horizontal Irradiance in Block 5 of the FACI.

Sitio	Puerto Bala	o (Ecuador)					
Fuente de datos	Fuente de datos Meteonorm 8.1 (2016-2021), Sat=100%						
	Irradiación horizontal global	Irradiación difusa horizontal	Temperatura	Velocidad del viento	Turbidez Linke	Humedad relativa	
	kWh/m²/día	kWh/m²/día	°C	m/s	[-]	%	
Enero	4.93	2.18	25.6	2.80	3.669	79.3	Datos regueridos
Febrero	4.92	2.83	25.8	2.20	3.994	82.7	Irradiación borizontal dobal
Marzo	5.17	2.78	26.1	2.20	4.146	82.0	Temperatura ext. promedio
Abril	5.64	2.72	25.6	2.39	4.074	82.6	-Dator adirionalar
Mayo	5.28	2.28	25.6	3.00	4.017	78.9	Irradiación difusa horizontal
Junio	4.79	2.41	24.3	3.40	4.051	81.5	Velocidad del viento
Julio	4.79	2.59	24.1	3.80	3.995	80.1	Turbidez Linke
Agosto	4.73	2.78	23.6	3.90	4.361	80.2	Humedad relativa
Septiembre	4.35	2.35	23.2	4.00	4.789	81.6	
Octubre	4.68	2.64	23.7	3.89	4.304	79.9	-Unidades de irradiación
Noviembre	4.85	2.44	23.7	3.90	4.324	80.2	NWh/m²/dia
Diciembre	5.11	2.52	25.1	3.60	4.054	76.2	O KWh/m*/mes
Año 🕜	4.94	2.54	24.7	3.3	4.148	80.4	O MJ/m²/mes
4.9	rradiación horiz	ontal global varia n/m /d	abilidad año a año ay²	6.9%			⊖ wr/m² O Índice de claridad Kt

Note. Taken from (Cagua, 2023).

In the following section of this article, the work of selecting the main components of the assisted photovoltaic system for Block 5 is carried out. This selection or identification of components, which could also be called sizing or design of the photovoltaic system, is carried out through the use of the PVsyst software. Basically, this sizing consists of entering in the software the parameters or characteristics related to the installation and operation of the photovoltaic system. Among the main parameters to be entered are: the optimal inclination of the photovoltaic modules, their orientation and output voltage, the power consumption of the load, and the system losses. The orientation and inclination of the photovoltaic modules (Figure 5) should be such that they receive as much energy as possible when they receive the sun's rays. The greatest amount of energy received by the modules is when the sun's rays strike perpendicularly on the solar cells of the panel (Institute of Educational Technologies, 2023). (Institute of Educational Technologies, 2023)... To achieve this, the orientation ($\mathbf{a} = Azimuth$) of the photovoltaic modules must be in the direction of the equator (parallel 0°). As the Block 5 building is located in Esmeraldas - Ecuador (northern hemisphere), the orientation of the photovoltaic modules must be towards the south, in other words, towards the equator, with an azimuth angle of 0° ($\mathbf{a} = 0^{\circ}$). On the other hand, the optimal tilt (βopt) of the modules can be determined through equation 1, as follows, where $\mathbf{\phi}$ is the latitude of the installation site (Rodriguez-Mas et al., 2022):

$$\beta_{opt} = 3.7 + 0.69 \cdot |\varphi|$$
 Eq.

Therefore:

$$\beta_{opt} = 3.7 + 0.69 \cdot |0.9721| = 4.37^{\circ}$$

Regarding the output voltage of the photovoltaic modules, it is recommended that. (Mascarós-Mateo, 2016; Ulloa-Santillán, 2020) that it be selected based on the information provided in Table 7.

Rated Working Voltage (V)	Cargo Demand
12 V	Less than 1500 W
12 V or 48 V	Between 1500 W and 5000 W
48 V or 120 V	Greater than 5000 W

 Table 7. Recommended output voltage levels for photovoltaic modules.

Note. Taken from (Cagua, 2023)

Losses in a photovoltaic installation can be of various types as shown in the example Loss Diagram in Figure 6, where an interconnected solar installation reinjects 1834 MWh to the electrical grid. Note that for this PV system the nominal power generated by the PV modules at standard test conditions (STC) is 2390 MWh. However, note that this input PV power, generated by the PV modules and transferred to the load, presents losses of various kinds that cause that, at the output of the PV system, a lower value of energy is obtained which is equal to 1834 MWh.

The sizing of the assisted photovoltaic system is done with the PVsyst software. In this software the meteorological data of the installation point are selected and the basic parameters of the PV system are also entered, which as mentioned in the previous section, are basically the following: a) inclination of the modules and their output voltage, b) demand of the fed load, c) losses of the PV system.

In the present study, we have determined that the optimal tilt of the PV modules is $\beta opt = 4.37^{\circ}$ and the orientation $\mathbf{a} = 0^{\circ}$ is southward (Figure 7). The total load demand has also been estimated to be a value of 25692 W using demand factors. Finally, as for the losses these have been defined with the default values set in PVsyst. With this information, the software allows the selection of the fundamental components of the system, which are the photovoltaic modules and inverters.

Figure 8 shows the window for selecting the key components (inverter and PV modules). In this window, the PV modules are selected with the criterion of having a high peak power level, since this reduces the number of modules needed to meet the building's demand. In addition, to comply with Table 7, the PV modules should have an output voltage between 48 to 120 V DC.

The selected inverter would be expected to be able to transfer all levels of input DC power to the AC load, regardless of irradiance and temperature conditions. However, in a real scenario, the PV system will operate at the highest DC power levels only on very occasional occasions throughout the year; for this reason, in order to reduce the cost of the inverter, it is generally recommended to undersize its respective output power. In other words, it is recommended to oversize the PV generator field with respect to the inverter output power. This concept is known as the Inverter Load Ratio (ILR) which is equal to the division between the input DC power (STC) of the PV system divided by the nominal AC output power of the inverter. According to (Masters & Hsu, 2023), in the United States normally an accepted value of ILR should be between 1 and 1.25. In the present study, an ILR of 1.2 is selected, i.e., the selected inverter is expected to be able to handle without overloading up to 80% of the maximum DC power level of the generator field. It is worth mentioning that an inverter normally has a mechanism that avoids overshooting the output power capacity by automatically limiting it to the nominal value whenever there is excess input power. The excess output power is not transferred by the inverter to the load and instead this device cuts the output power so that it does not exceed the nominal power. This behavior in the inverter is referred to as "clipping." (Good & Johnson, 2016; Masters & Hsu, 2023; Sandia National Laboratories, 2024)..

Figure 5. Orientation (angle α) and tilt (angle β) of a Photovoltaic Module.



Note. Taken from (Rodríguez-Mas et al., 2022)..

Figure 6. Example of losses of a solar PV system interconnected to the grid.



Note. Taken from (Diaz-Santos et al., 2017)..

🥌 Orientación, Variante "Nueva variante d	le simulación"	– 🗆 X
Tipo de campo [Plano inclinado fijo 📉 🗹	
Parámetros del campo	Incline 4°	Azimat 0°
Azimut 0.0	Panel inclination	Ojeste Este
		Sur
–Optimización rápida		×
Optimización con respecto a		Orientation: South
Rendimiento irradiación anu	•	
O Verano (abr-sept)	1.2	1.2
O Invierno (oct-mar)	t t	ANO L
Bandimianta matao anual	1.0	
	0.8 ETrappos = 1.00	- 0.8
Pérdida con respecto al óntimo	Pérdida/opt.= 0.0	
Global en el plano colector 1808 k	Wh/m ² 0.6 0 30 60 100 100 100 100 100 100 100 100 100	90 -90 -60 -30 0 30 60 90
		Y Cancelar

Figure 7. Entry of PV module tilt and orientation parameters in PVsyst.

Note. Taken from (Cagua, 2023).

Figure 8. Selection of the technical specifications of the main components of the block 5 assisted photovoltaic system.

r	Definición del sistema de red, Variante VCO: "Nueva variante de simulación" Potonocia, planoa d	2	-	□ x
	Subconjunto	c Lista de subconjuntos		0
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	Criente Plano inclinado fijo Inclinación 4º Azimut 0º Redmens o área disponible(módulos) 0 132 m²	Nombre	#Mód #Inv.	#Cadena #MPPT
<	Seleccione el módulo IV Costo de 1970 - Intro Todos los módulos F Modulos recesarios aprox. 79 Panasonic 330 Wp 49V HIT V8HV 330-5147 Desde 2023 Detasteets 2023 C Abrir	Generador FV Bloque S Panasonic - VBHN-330-5347 Fronius International - ECO 25.0-3-	12 1	6 1
	Selección del módulo FV keje: Vinpo (60°C) 51.3 V Vec(10°C) 75.5 V			
<	Seleccione el inversor			
	Fronks: International 25 kW 580 - 850 V TL 50/60 H: ECO 25.0-3-5 Deside 2015 Q Atrir Núm. de inversores 0 2 Valtaje de funcionamiento: 580-850 V Poder global inversor 25.0 Wica			
	Voltaje máximo de entrada: 1000 V Inversor "String" con 6 entradas Selección del inversor			
	Diseñe el conjunto Diseñe el conjunto Definición de la cantidad de cadenas y módulos.			
	Condiciones de operación sobredmensionada.	Resumen sistema global		
	Mód. en serie 12 0 ♥ whtre 12 y 13	Núm. de módulos 72 Área del módulo 121 m ²		
	Nán. cedenas 6 © @ entre 6 y 9 Predis cercargo 80 % Temensionamiento #0 Pagoción Promo Sector 4 (en 100 W/m² Construction 4 (en 100 W/m² Con	Núm. de inversores 1 Potencia FV nominal 23.8 kWp Potencia de CA nominal 25.0 kWCA Pronerción Prom 0.950		
	Núm. de módulos 72 Área 121 m ² Isc (en STC) 36.4 A Potencia nom. conjunto (STC)23.8 kWp			
	Q Resumen del sistema 🛛 🛞 Diagrama unifilar	🗶 Cancelar	-	ок

Table 8 presents a summary of the sizing of the assisted photovoltaic system for Block 5. This table shows the fundamental components of the system and also mentions other aspects related to the design of the photovoltaic field; for example, the number of modules required, the configuration of the photovoltaic array, the power generated, etc., are determined.

Note in Table 8, that an area of 121 m2 is required for the installation of the 72 solar panels needed by the assisted photovoltaic system. It has been determined that the terrace of Block 5 has an available area of approximately 600 m2; therefore, there is sufficient area to implement the photovoltaic field (photovoltaic modules) on the terrace of this building.

Description	Manufactur er	Model	Features
PV modules	Panasonic	VBHN-330- SJ47	Rated power (STC): 330 Wp V _{MPP} @ 60 °C: 51.3V
Inverter	Fronius Internation al	ECO 25.0-3- S	Rated power: 25kW Input voltage: 580 - 850V
Photovoltaic field design	N/A	N/A	Modules in series: 12 Strings: 6 Number of modules: 72 Area covered by modules: 121 m ² Rated power of photovoltaic field (STC): 23.8 kWp

 Table 8. Technical specifications of the assisted photovoltaic system.

Note. Based on (Cagua, 2023).

Results

Once the key components of the system have been dimensioned in PVsyst (Figure 8) and the self-consumption needs for the building load have been established (Figure 9), the PV system performance simulation is run in PVsyst. The result of the simulation is the "PVsyst - Simulation Report" (Figures 10 and 11) which indicates various details related to the performance of the assisted PV system.

Among the information presented on page 5 of the PVsyst simulation report (Figure 11), it is possible to identify that the annual consumption of the load is 225044 kWh. Additionally, it can be observed that the PVsyst system contributes 36973 kWh to the load, while the grid provides the remaining energy, i.e. 188071 kWh. This means that, once the assisted PV system is implemented, about 20 % of the total energy to power the load will come from the solar panels

throughout the year. Logically, this would represent a 20% reduction in energy consumption from the grid. This fact means that an economic saving of the same percentage (20%) would be expected in the monthly energy consumption bills of this building once the assisted photovoltaic system is implemented.

Finally, Table 9 shows an approximate budget for the materials, main equipment and services required to build the assisted photovoltaic system that we have studied in this article.

🗣 Definición de necesidades del usuarioVariante: "Nueva variante de	simulación", Variant "Nueva variante de simulación" — 🛛 🗙
Comentario Nuevo Necesidades del dudarovariante in Nueva variante del Comentario Nuevo Necesidades Del Domando O Garacterísticas generales Sin autoconsumo © Consumo constante fijo O Valores mensuales O Perfiles diarios O Perfiles de probabilidad O Consumidores domésticos O Cargar valores de un archivo CSV por hora/diario (?)	Sincladori, variance volgeve variance de sincladori f Block 5- FACI: 25692W
Q Resumen del sistema	Emprimir K Cancelar VK

Figure 9. Entry of self-consumption parameters in PVsyst.

Note. Taken from (Cagua, 2023).

Figure 10. PVsyst simulation report (page 1).



Note. Taken from (Cagua, 2023).

Figure 11. Production of the assisted photovoltaic system.



Note. Taken from (Cagua, 2023).

Table 9.	Approximate	budget of	the assi	sted photo	ovoltaic sys	stem for
Block 5 -	- FACI.					

	Assisted Photovoltaic System Budget					
No.	Description	Quantity	Unit	Unit Cost	Total Value	
1	330 Wp photovoltaic module. Manufacturer: Panasonic. Model: VBHN-330-SJ47	72	EA	\$320,00	\$23.040,00	
2	Inverter 25 kW. Manufacturer: Fronius International. Model: ECO 25.0-3-S	1	EA	\$3.500,00	\$3.500,00	
3	Structure	1	GB	\$1.800,00	\$1.800,00	
4	Grounding rod.	1	EA	\$16,00	\$16,00	
5	General switch.	1	EA	\$35,00	\$35,00	
6	Differential switch of 30 mA sensitivity.	1	EA	\$12,00	\$12,00	
7	gPV fuses.	8	EA	\$8,00	\$64,00	
8	Photovoltaic Cable. 300 meters.	1	EA	\$1.062,00	\$1.062,00	
9	MC4 connectors.	150	EA	\$7,14	\$1.071,00	
10	SPD (varistors).	5	EA	\$35,12	\$175,60	
11	Labor.	1	GB	\$2.000,00	\$2.000,00	
				Total Power (W)	\$32.775,60	

Note. Taken from (Cagua, 2023)

Conclusions

The use of specialized tools such as PVsyst has made it possible to predict the performance of an assisted photovoltaic system designed for the FACI Block 5 building. Through the use of this software it has been possible to select the essential components of this type of photovoltaic system, such as the photovoltaic modules and the inverter. The results obtained in the PVsyst simulation report support the design decisions and ensure the efficiency of the proposed system.

On the other hand, meteorological and geolocation information has been used in this study, and at the same time information has been gathered through visual inspections of the installation site, in order to evaluate whether the conditions are favorable to support the implementation of the project in a technical manner.

In addition, the detailed study of the installed load in the "Block 5" building has revealed crucial information to determine the energy demand. This step has been essential to properly size the PV-assisted system, ensuring that it can meet the needs efficiently. Effective planning has been made possible by understanding consumption patterns and projecting solar power generation. A detailed budget has also been prepared considering the costs associated with equipment acquisition and installation.

To conclude, the results of this work have supported the feasibility of implementing an assisted photovoltaic system in Block 5. The detailed identification of the technical specifications of the main components, the accurate identification of the load and the presentation of a detailed budget form a comprehensive framework for the successful implementation of the project.

This work lays the groundwork for the transition to a more sustainable energy source in Block 5, and also suggests that the adoption of solar energy will not only be beneficial from an environmental standpoint, but may also have a positive impact on long-term cost reduction.

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